

Near-field Liquid Crystal RIS Phase-Shift Design for Secure Wide-band Illumination



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2- LC Model

3- Secure Wideband Illumination

4- Performance Evaluation

5- Conclusions

6- References

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Introduction

Motivation

- Demands:
Higher data rates and capacity are required in modern communication systems (e.g., 5G, 6G).
- To provide higher data rates, expanding available **bandwidth** through increased **frequency** is essential.

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Time	XG	Aim	Data rate
1979	1G	Voice	2 - 3 kbps
1991	2G	SMS	20 - 40 kbps
1998	3G	Data	0.5 - 3 Mbps
2009	4G	Streaming	20 - 100 Mbps
2019	5G	Sensing	100 - 400 Mbps
2030	6G	Intelligence	1 - 10 Gbps

Introduction

RIS Implementation

	Varactor	PIN Diode	MEMS Switch	MEMS Mirror	LC
Tuning time	ns	ns	μ s	100s of μ s	> 10 ms
Tunability	continuous	discrete (1 bit/diode)	discrete	discrete	continuous
Power consumption	medium	medium	low	low	low
Scalability	low (cost per diode)	low (cost per diode)	medium (encapsulation)	medium (cost per area)	high
Frequency range	few GHz	mm-Wave	mm-Wave	THz	> 10 GHz
Cost	high	high	high	high	low

Comparison of technologies used for the realization of RIS [1].

[1] Alejandro Jiménez-Sáez et al. "RISs with LC Technology: A Hardware Design and Communication Perspective". In: arXiv:2308.03065 (2023).

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LC Model

LC Model

$$[\omega(f_k)]_n = \left(1 + \beta\left(\frac{f_k}{f_c} - 1\right)\right) [\omega_c]_n, \forall n, \forall k,$$

- f_c : Center frequency,
 f_k : k th subcarrier,
 $[\omega_c]_n$: RIS phase shifter in n th element and f_c ,
 β : A physical constant parameter.

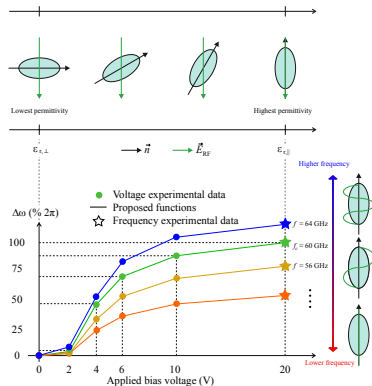
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Secure Wideband Illumination

System Model and Problem

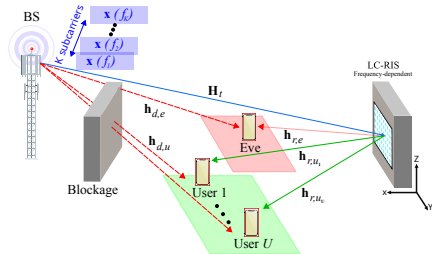


Figure: $\mathcal{P}_u$ and $\mathcal{P}_e$ are the green and red areas, respectively.

Secure Wideband Illumination

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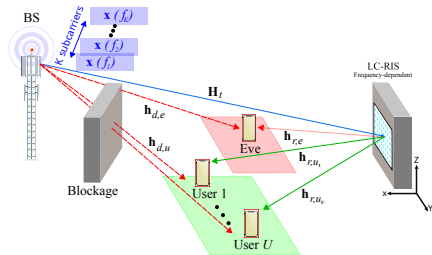


Figure: $\mathcal{P}_u$ and $\mathcal{P}_e$ are the green and red areas, respectively.

$$\begin{aligned}
 \text{P1: } & \max_{\alpha, \omega_c, \mathbf{q}} \alpha \\
 \text{s.t. } & \text{SR}(f_k) \geq \alpha, \forall \mathbf{p}_u \in \mathcal{P}_u, \forall \mathbf{p}_e \in \mathcal{P}_e, \forall k, \\
 & 0 \leq [\omega_c]_n < 2\pi, \\
 & [\omega(f_k)]_n = [\omega_c]_n \beta_k, \forall n, \forall k, \\
 & \|\mathbf{q}\|_2^2 \leq P_t.
 \end{aligned}$$

$$\text{SR}(f_k) = [\log(1 + \text{SNR}_u(f_k)) - \log(1 + \text{SNR}_e(f_k))]^+,$$

$$\text{SNR}_u(f_k) = |(\mathbf{h}_u^{\text{eff}}(f_k))^H \mathbf{q}|^2 / \sigma_n^2,$$

$$\text{SNR}_e(f_k) = |(\mathbf{h}_e^{\text{eff}}(f_k))^H \mathbf{q}|^2 / \sigma_n^2,$$

Secure Wideband Illumination

Impact of the Number of Tx Antennas on Beam Squinting

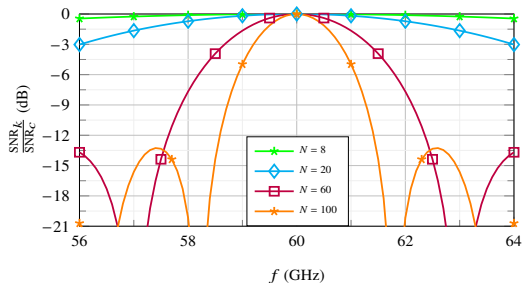


Figure: The normalized Rx power (dB) versus frequency for given N values 8, 20, 60, and 100.

Secure Wideband Illumination

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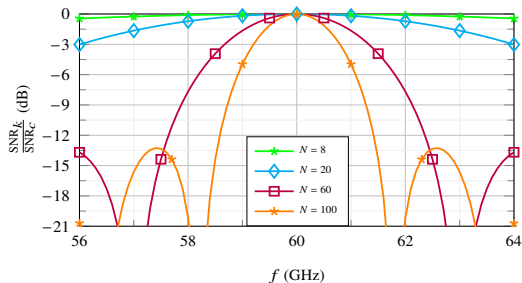


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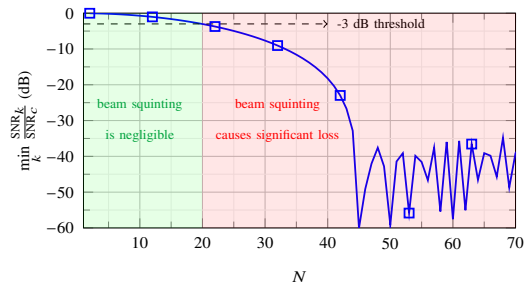


Figure: The normalized minimum Rx power (dB) across all subcarriers versus number of Tx antenna for given bandwidth 8.64 GHz, where $f_c = 60$ GHz.

Secure Wideband Illumination

Beamformer Design

$$\begin{aligned} \text{P2: } \quad & \max_{\alpha, \mathbf{q}} \alpha \\ \text{s.t. } \quad & \text{SR}(f_k) \geq \alpha, \forall \mathbf{p}_u \in \mathcal{P}_u, \forall \mathbf{p}_e \in \mathcal{P}_e, \forall k, \\ & \|\mathbf{q}\|_2^2 \leq P_t. \end{aligned}$$

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Beamformer Design

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Lemma

Assuming a dominant LOS link, fixed RIS phase shifts, and blocked direct channels for both the legitimate user and the eavesdropper, the optimal beamformer for P2 is given by $\mathbf{q} = \sqrt{P_t} \mathbf{a}_{\text{BS}}(\mathbf{p}_{\text{RIS}}, f_c)$, where $\mathbf{a}_{\text{BS}}$ is steering vector in BS and $\mathbf{p}_{\text{RIS}}$ is the RIS location.

Proof.

The proof is provided in [3, Lemma 1]. □

[3] Mohamadreza Delbari, et al. "Temperature-aware phase-shift design of LC-RIS for secure communication". In: ICC (2025).

Secure Wideband Illumination

RIS Phase Shifter Design

$$\begin{aligned} \text{P3: } & \max_{\alpha, \boldsymbol{\omega}_c} \alpha \\ \text{s.t. } & \text{SR}(f_k) \geq \alpha, \forall (\mathbf{p}_u, \mathbf{p}_e) \in \mathcal{P}_u \times \mathcal{P}_e, \forall k, \\ & 0 \leq [\boldsymbol{\omega}_c]_n < 2\pi, \\ & [\boldsymbol{\omega}(f_k)]_n = [\boldsymbol{\omega}_c]_n \beta_k, \forall n, \forall k. \end{aligned}$$

Secure Wideband Illumination

RIS Phase Shifter Design

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$$\text{P4: } \max_{\gamma, \mathbf{S}_c} \gamma$$

$$\begin{aligned} \text{s.t. } & \text{C1: } \text{tr}(\mathbf{A}_k(\gamma) \mathbf{S}_c^{\circ \beta_k}) \geq \gamma - 1, \forall (\mathbf{p}_u, \mathbf{p}_e) \in \mathcal{P}_u \times \mathcal{P}_e, \forall k, \\ & \text{C2: } \mathbf{S}_k \succeq \mathbf{0}, \forall k, \\ & \text{C3: } \text{rank}(\mathbf{S}_k) = 1, \forall k, \\ & \text{C4: } \text{diag}(\mathbf{S}_k) = \mathbf{1}_N, \forall k, \end{aligned}$$

$$\begin{aligned} \text{where } & \log(\gamma) = \alpha, \quad \mathbf{s}_k \triangleq [\mathbf{e}^{j[\boldsymbol{\omega}(f_k)]_1}, \dots, \mathbf{e}^{j[\boldsymbol{\omega}(f_k)]_N}]^T, \forall k, \quad \mathbf{S}_c^{\circ \beta_k} \triangleq \mathbf{s}_k \mathbf{s}_k^H, \forall k, \text{ and} \\ & \mathbf{A}_k(\gamma) \triangleq \mathbf{A}_k^u(\mathbf{p}_u) - \gamma \mathbf{A}_k^e(\mathbf{p}_e), \quad \mathbf{A}_k^g = \frac{\text{diag}(\mathbf{h}_{r,g}(f_k)^H) \mathbf{H}_t(f_k) \mathbf{q} \mathbf{q}^H \mathbf{H}_t(f_k)^H \text{diag}(\mathbf{h}_{r,g}(f_k))}{\sigma_n^2}, g = \{u_1, \dots, u_U, e\}. \end{aligned}$$

Secure Wideband Illumination

RIS Phase Shifter Design

$$\text{P5: } \max_{\gamma, \mathbf{S}_c} \gamma$$

$$\text{s.t. } \mathbf{C1}, \widehat{\mathbf{C2}} : \mathbf{S}_c \succeq 0,$$

$$\widehat{\mathbf{C3}} : \text{rank}(\mathbf{S}_c) = 1, \widehat{\mathbf{C4}} : \text{diag}(\mathbf{S}_c) = \mathbf{1}_N.$$

Proof.

It can be proved by [4, Lemma 2]. $\square$

[4] Mohamadreza Delbari, et al. "Near-field Liquid Crystal RIS Phase-Shift Design for Secure Wideband Illumination". In: arXiv:2508.04331 (2025).

Secure Wideband Illumination

RIS Phase Shifter Design

$$\text{P5: } \max_{\gamma, \mathbf{S}_c} \gamma$$

$$\text{s.t. } \widehat{\mathbf{C}}1, \widehat{\mathbf{C}}2 : \mathbf{S}_c \succeq 0,$$

$$\widehat{\mathbf{C}}3 : \text{rank}(\mathbf{S}_c) = 1, \widehat{\mathbf{C}}4 : \text{diag}(\mathbf{S}_c) = \mathbf{1}_N.$$

$$\text{P6: } \max_{\gamma, \mathbf{S}_c} \gamma - \eta^{(i)} \left(\|\mathbf{S}_c\|_* - \|\mathbf{S}_c^{(i)}\|_2 - \text{tr}(\boldsymbol{\lambda}_{\max}(\mathbf{S}_c^{(i)}), \right. \\ \left. \times \boldsymbol{\lambda}_{\max}^H(\mathbf{S}_c^{(i)})(\mathbf{S}_c - \mathbf{S}_c^{(i)})) \right)$$

$$\text{s.t. } \widehat{\mathbf{C}}1, \widehat{\mathbf{C}}2, \widehat{\mathbf{C}}4.$$

Proof.

It can be proved by [4, Lemma 2]. $\square$

where $\widehat{\mathbf{C}}1$ is:

$$\text{tr} \left(\mathbf{A}_k(\gamma) \left(\left(\mathbf{S}_c^{(i)} \right)^{\circ(\beta_k)} + \left(\beta_k \left(\mathbf{S}_c^{(i)} \right)^{\circ(\beta_k-1)} \right) \odot \left(\mathbf{S}_c - \mathbf{S}_c^{(i)} \right) \right) \right) \\ \geq \gamma - 1, \forall (\mathbf{p}_u, \mathbf{p}_e) \in \mathcal{P}_u \times \mathcal{P}_e, \forall k.$$

[4] Mohamadreza Delbari, et al. "Near-field Liquid Crystal RIS Phase-Shift Design for Secure Wideband Illumination". In: arXiv:2508.04331 (2025).

Secure Wideband Illumination

Solution

Two optimization variables γ and $\mathbf{S}_c$:
-> Alternative Optimization

[5] Grant, Michael. "CVX: Matlab software for disciplined convex programming, version 1.21," <http://cvxr.com/cvx> (2014).

Secure Wideband Illumination

Solution

Two optimization variables γ and $\mathbf{S}_c$:
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When γ is fixed:

Problem P6 can be solved using standard convex optimization solvers, e.g., CVX [5].

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Solution

Two optimization variables γ and $\mathbf{S}_c$:
-> Alternative Optimization

When γ is fixed:

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When $\mathbf{S}_c$ is fixed:

$$\gamma = \min_{\forall \mathbf{p}_u \in \mathcal{P}_u, \forall \mathbf{p}_e \in \mathcal{P}_e, \forall k} \frac{\text{tr}(\mathbf{A}_k^u(\mathbf{p}_u)\mathbf{S}_k) + 1}{\text{tr}(\mathbf{A}_k^e(\mathbf{p}_e)\mathbf{S}_k) + 1}.$$

[5] Grant, Michael. "CVX: Matlab software for disciplined convex programming, version 1.21," <http://cvxr.com/cvx> (2014).

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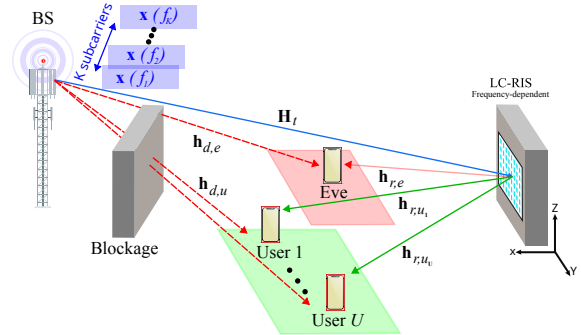
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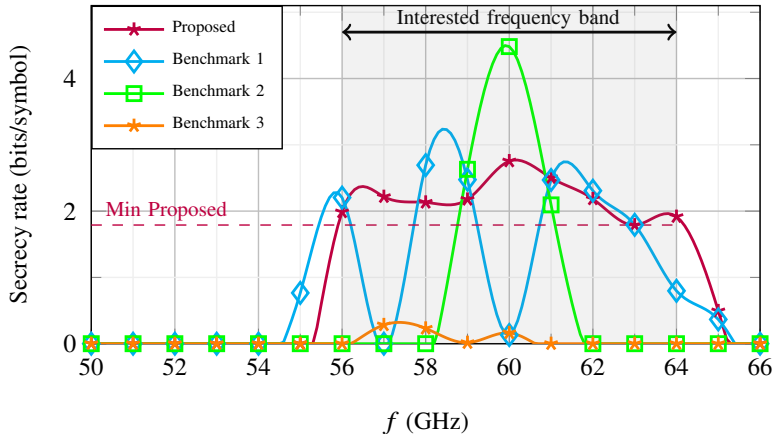
Simulation Setup

Parameter	Value
Frequency	60 GHz
Bandwidth	8.64 GHz
Transmission Power	43 dBm
BS Antennas (x – z axes)	16×16
RIS Elements (y-axis)	100
Channel Model	Ricean
Path Loss Model	$(c/(4\pi f_k d))^2$
Noise Level	-95 dBm
Direct Blockage	- 40 dB
β	2.4



Performance Evaluation

Simulation Result



Performance Evaluation

Simulation Result

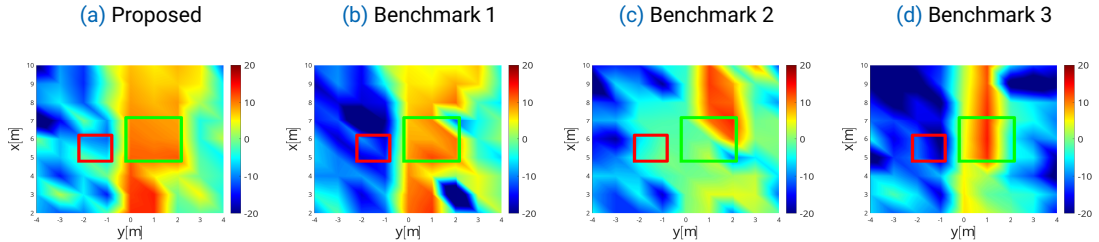
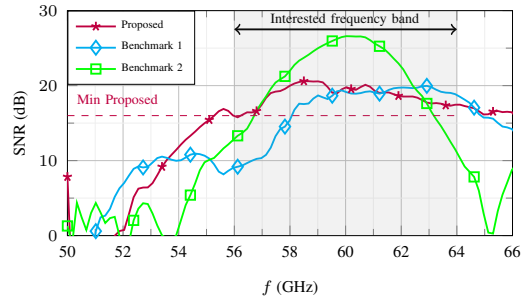
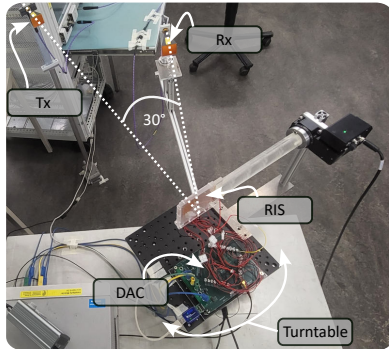


Figure: SNR (dB) using four different methods at $f_k = 57$ GHz. The green area represents the user coverage region, while the red area indicates the possible locations of the eavesdropper.

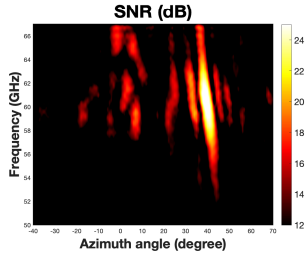
Performance Evaluation

Experimental Results

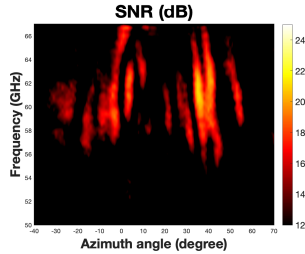


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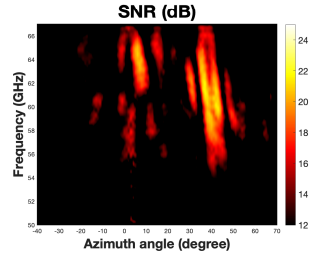
Experimental Results



(a) Benchmark 2



(b) Benchmark 1



(c) Proposed

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Conclusions

Summary and takeaways

Summary:

- We need higher frequencies, and LCs are one potential way for implementation.
- Despite being good candidates to implement RISs, LC's RIS phase shifters are frequency-dependent.
- We derived a frequency model of the LC RIS phase shifters.
- We have optimized LC-RIS phase shifts in the secure communication scenario by considering the frequency dependency.

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- Despite being good candidates to implement RISs, LC's RIS phase shifters are **frequency-dependent**.
- We derived a **frequency model** of the LC RIS phase shifters.
- We have optimized LC-RIS phase shifts in the secure communication scenario by **considering the frequency dependency**.

Future research directions:

- Developing a scalable solution since the complexity of the current algorithm is $\mathcal{O}(I_{\max}|\mathcal{P}_u||\mathcal{P}_e|N^3K)$.

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Delbari, Mohamadreza, et al. "Temperature-aware phase-shift design of LC-RIS for secure communication." ICC IEEE, 2025.



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Thank you for your attention!

Questions?

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